



# HIT-RE 500 V4 INJECTION MORTAR

**Product Technical Datasheet**  
**Concrete-to-concrete**  
Update: July 24



# HIT-RE 500 V4 injection mortar

Rebar design (EN 1992-1-1, EOTA TR 069, EN 1998-1) / Rebar elements / Concrete

## Injection mortar system




HIT-RE 500 V4

(Available in 330-, 500- and 1400-ml Foil pack)



Rebar  
( $\phi 8$  -  $\phi 40$ )

## Benefits

-  technology: Simplified method of borehole preparation using either Hilti hollow drill bit for hammer drilling or Roughening tool for diamond cored applications.
- Allows the design of post-installed, moment-resisting reinforced concrete connections under static loading conditions without using a splice configuration according to TR 069
- Suitable for concrete C 12/15 to C 50/60
- ETA Data for 100 years working life
- High loading capacity
- Suitable for dry and water saturated concrete
- Non-corrosive to rebar elements
- Long working time at elevated temperatures
- Cures down to  $-5^{\circ}\text{C}$  concrete temperature.
- Odourless epoxy



## Application condition

### Base material

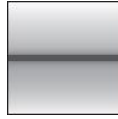


Concrete (non-cracked)

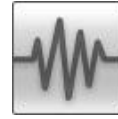


Concrete (cracked)

### Load conditions



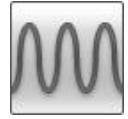
Static/  
quasi-static



Seismic

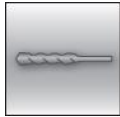


Fire resistance



Fatigue

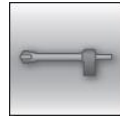
### Installation conditions



Hammer drilling



Diamond cored



Hollow drill bit drilling



Water-filled boreholes

### Other information



ETA Working life 100 years



PROFIS Engineering design Software



Concrete-to-Concrete connections Handbook

## Linked Approvals/Certificates and Instructions for use.

### Approvals / Certificates

Approval no.	Application / Loading condition	Authority / Laboratory	Date of issue	Date of expiry
<a href="#">ETA-20/0540</a>	Static and quasi-static / Seismic / Fire	CSTB, Marne la Vallée	13-12-2023	-
<a href="#">ETA-20/0539</a>	Static and quasi-static / Seismic	CSTB, Marne la Vallée	13-12-2023	-
Z-21.8-2123	Fatigue loading- German National Approval	DIBt, Berlin	28-01-2021	28-01-2026
No.: 07/2021	Engineering Judgement (120-y working life based on EAD 330087-01-0601)	BERMEIGSTER, Vienna	19-07-2021	-
No.: 04/2022	Engineering Judgement (120-y working life based on EAD 332402-00-0601-v01)	BERMEIGSTER, Vienna	08-03-2022	-

### Instructions for use(IFU)

Material				
Injection mortar	<a href="#">IFU Hilti HIT-RE 500 V4 (330/500 ml)</a>		<a href="#">IFU Hilti HIT-RE 500 V4 (1400 ml)</a>	
Dispenser	<a href="#">IFU HDM</a>	<a href="#">IFU HDE 500-22</a>	<a href="#">IFU HDE 500-A12</a>	<a href="#">IFU HIT-P8000D</a>

### Link to Hilti Webpage

Injection mortars / Dispenser				
<a href="#">Hilti HIT-RE 500 V4</a>	<a href="#">HDE 500-22</a>	<a href="#">HDE 500-A12</a>	<a href="#">HDM 500</a>	<a href="#">P8000D</a>

### Mechanical properties and dimensions rebar

Mechanical properties and dimensions of the rebars are standardized and can be taken from the ETA.

### Material quality

Part	Material
Rebar EN 1992-1-1:2004	Bars and de-coiled rods class B or C according to NDP or NCL of EN 1992-1-1/NA

**Static and quasi-static loading as per ETA 20/0540. Design according to EN 1992-1-1**

**All data in this section applies to:**

- According to EN 1992-1-1 for good bond conditions. For all other bond conditions multiply the values by 0,7
- Hammer drilling, Hammer drilling with Hilti hollow drill bit (TE-CD, TE-YD), Compressed air drilling
- Diamond coring (dry) ,Diamond coring with roughening with Hilti Roughening tool TE-YRT
- Design values of the bond strength for a working life of 50 Years

For specific design cases refer to [PROFIS Engineering](#)

**Design bond strength in N/mm<sup>2</sup> for above methods of drilling techniques according to mortar IFU & ETA-20/0540.**

Rebar size [mm]	Concrete class								
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
	$f_{bd,PIR}$ [N/mm <sup>2</sup> ]								
φ8 - φ32	1,6	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
φ34	1,6	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
φ36	1,6	1,9	2,2	2,6	2,9	3,2	3,5	3,8	4,1
φ40	1,5	1,8	2,1	2,5	2,8	3,1	3,4	3,7	3,9

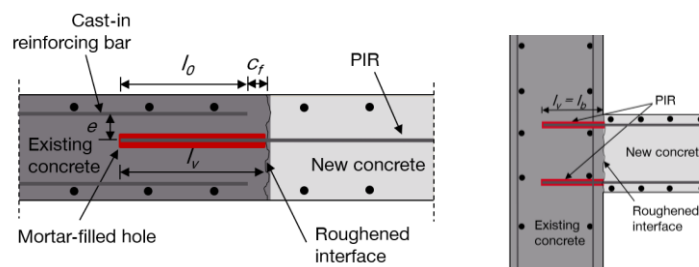
**Minimum anchorage length and minimum lap length**

Post-installed rebar applications as per EN 1992-1-1	Typical examples
Lap splice applications	
End anchorage applications – simply supported / compression load-only connections	

The minimum anchorage length  $l_{b,min}$  and the minimum lap length  $l_{0,min}$  according for applications designed as per EN 1992-1-1 shall be multiplied by relevant **Amplification factor**  $\alpha_{lb}$  in the table below.

**Amplification factor  $\alpha_{lb}$  for the min. anchorage length and min. lap length according to mortar IFU & ETA-20/0540.**

Rebar size [mm]	Concrete class								
	C12/15	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
	$\alpha_{lb}$ [-]								
φ8 - φ40	1,0								



Refer to the table for data on dispensers and corresponding maximum embedment depth  $l_{v,max}$  due to mortar installation limitations



**Anchorage length and lap length for characteristic steel strength  $f_{yk} = 500 \text{ N/mm}^2$  for good bond conditions**

- $l_{b,min}$  Minimum anchorage length for simply supported connections under tension loading assuming  $\sigma_{sd} = f_{yd}$
- $l_{o,min}$  Minimum anchorage length for overlap splice joint
- $l_{bd,y}$  Anchorage length for simply supported connections (design for yielding)
- $l_{o,PIR,y}$  Anchorage length for overlap joint (design for yielding)
- $\alpha_2$  Coefficient of Concrete Cover

For specific design cases refer to [PROFIS Engineering](#)

For detailed technical contents, refer to [Concrete-to-Concrete connections Handbook](#)

Rebar-size [mm]	Concrete class	Design Resistance (Yielding) [kN]	$l_{b,min}$ [mm]	$l_{o,min}$ [mm]	$l_{bd,y}$ ( $\alpha_2=1$ ) [mm]	$l_{bd,y}$ ( $\alpha_2=0,7$ ) [mm]	$l_{o,PIR,y}$ ( $\alpha_2=1$ ) [mm]	$l_{o,PIR,y}$ ( $\alpha_2=0,7$ ) [mm]
$\phi 8$	C20/25	21,9	113	200	378	265	567	398
	C50/60		100	200	202	142	303	213
$\phi 10$	C20/25	34,1	142	213	473	331	710	497
	C50/60		100	200	253	177	380	266
$\phi 12$	C20/25	49,2	170	255	567	397	851	596
	C50/60		120	200	303	212	455	318
$\phi 14$	C20/25	66,9	198	298	662	463	993	695
	C50/60		140	210	354	248	531	372
$\phi 16$	C20/25	87,4	227	340	756	529	1134	794
	C50/60		160	240	404	283	606	425
$\phi 20$	C20/25	136,6	284	426	945	662	1418	993
	C50/60		200	300	506	354	759	531
$\phi 25$	C20/25	213,4	354	532	1181	827	1772	1241
	C50/60		250	375	632	442	948	663
$\phi 28$	C20/25	267,7	397	596	1323	926	1985	1389
	C50/60		280	420	708	495	1062	743
$\phi 30$	C20/25	307,3	425	638	1418	992	2127	1488
	C50/60		300	450	758	531	1137	797
$\phi 32$	C20/25	349,7	454	681	1512	1059	2268	1589
	C50/60		320	480	809	566	1214	849
$\phi 34$	C20/25	394,7	482	723	1608	1125	2411	1688
	C50/60		340	510	880	616	1321	924
$\phi 36$	C20/25	442,6	534	801	1779	1245	2669	1868
	C50/60		360	540	954	668	1431	1002
$\phi 40$	C20/25	546,4	621	932	2070	1449	3105	2174
	C50/60		400	600	1115	780	1673	1170

**Seismic loading based on ETA-20/0540. Seismic design according to EN 1998-1**

**All data in this section applies to:**

- According to EN 1992-1-1 for good bond conditions. For all other bond conditions multiply the values by 0,7
- Hammer drilling, Hammer drilling with Hilti hollow drill bit (TE-CD, TE-YD) ,Compressed air drilling
- Diamond coring (dry),Diamond coring with roughening with Hilti Roughening tool TE-YRT
- Design values of the bond strength for a working life of 50 Years

For specific design cases refer to [PROFIS Engineering](#)

For detailed technical contents, refer to [Concrete-to-Concrete connections Handbook](#)

**Design bond strength in N/mm<sup>2</sup> for good bond conditions for above methods of drilling techniques according to mortar IFU & ETA-20/0540**

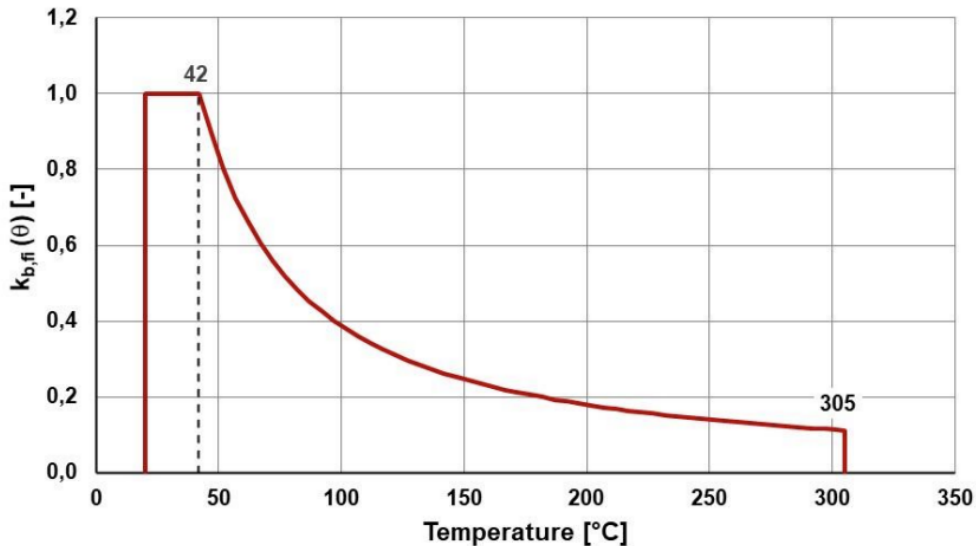
Rebar Size	Concrete class							
	C16/20	C20/25	C25/30	C30/37	C35/45	C40/50	C45/55	C50/60
[mm]	f <sub>bd,PIR,seis</sub> [N/mm <sup>2</sup> ]							
φ8 - φ32	2,0	2,3	2,7	3,0	3,4	3,7	4,0	4,3
φ34	2,0	2,3	2,6	2,9	3,3	3,6	3,9	4,2
φ36	1,9	2,2	2,6	2,9	3,2	3,5	3,8	4,1
φ40	1,8	2,1	2,5	2,8	3,1	3,4	3,7	3,9

## Fire resistance based on ETA-20/0540 for working life of 50 years

For evidence under fire exposure the anchorage length shall be calculated according to EN 1992-1-1:2004+AC:2010 Equation 8.3 using the temperature-dependent bond resistance  $f_{bd,fi}$ .

For specific design cases refer to [PROFIS Engineering](#)

### Temperature reduction factor $k_{fi}(\theta)$ for concrete class C20/25 for good bond conditions



The design value of the bond strength  $f_{bd,fi}$  under fire exposure have to be calculated by the following equation:

$$f_{bd,fi} = k_{b,fi}(\theta) \cdot f_{bd,PIR} \cdot \frac{\gamma_c}{\gamma_{M,fi}}$$

With  $\theta \leq 305^\circ\text{C}$ : 
$$k_{b,fi}(\theta) = \frac{651,24 \cdot \theta^{-1,115}}{f_{bd,PIR} \cdot 4,3} \leq 1,0$$

$\theta > 305^\circ\text{C}$  
$$k_{fi}(\theta) = 0,0$$

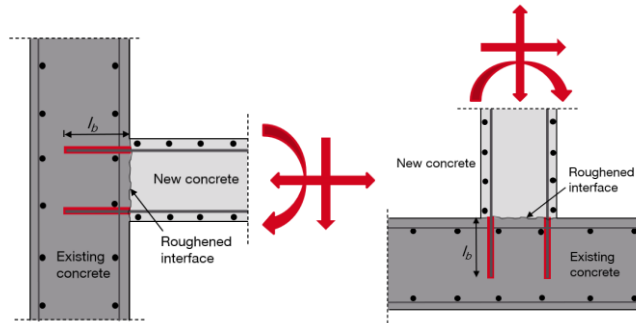
- $f_{bd,fi}$  = Design value of the bond resistance in case of fire in N/mm<sup>2</sup>
- $\theta$  = Temperature in °C in the mortar layer
- $k_{b,fi}(\theta)$  = Reduction factor under fire exposure
- $f_{bd,PIR}$  = Design value of the bond resistance in N/mm<sup>2</sup> in cold condition considering the concrete classes, rebar diameter, the drilling method, and the bond conditions according to EN 1992-1-1
- $\gamma_c$  = Partial safety factor according to EN 1992-1-1
- $\gamma_{M,fi}$  = Partial safety factor according to EN 1992-1-2

### Bond strength $f_{bd,fi}$ in N/mm<sup>2</sup> for fire design for concrete classes C20/25 to C50/60

Rebar Temperature	50°C	100°C	150°C	200°C	250°C	305°C ( $\theta_{max}$ )
$f_{bd,fi}$ [N/mm <sup>2</sup> ]	2,90	1,34	0,85	0,62	0,48	0,39

**Static and quasi-static loading as per ETA 20/0539. Design according to EOTA TR 069**

For post-installed rebar solutions beyond provisions of EN 1992-1-1, such as end-anchorage applications with bi-axial and uni-axial bending and shear loads with compression or tension forces without the limitation of using strut-and-tie design approach can be designed using EOTA TR 069



**Anchorage length  $l_{bd,y}$  as per EOTA TR 069 design provisions (Improved bond-splitting failure mode) for characteristic steel strength  $f_{yk}=500 \text{ N/mm}^2$  for good bond conditions**

**All data in this section applies to**

- Hammer drilling,
- Effect of transverse reinforcement is not considered
- Effect of sustained loads are not considered
- Minimum spacing between rebars considered as 100 mm
- Minimum anchorage length  $l_{b,min}$  shall apply as per EN 1992-1-1
- The maximum recommended installation length shall be applicable
- Concrete breakout resistance is not considered (it shall be calculated depending on the boundary conditions of the actual concrete application)
- In-service temperature range I (min. base material temperature  $-40^\circ\text{C}$ , max. long/short term base material temperature:  $+24^\circ\text{C}/+40^\circ\text{C}$ )
- Material and installation factors:  $\gamma_{Ms}=1,15$  ,  $\gamma_{Mc}=1,5$  ,  $\gamma_{inst}=1,0$
- Minimum concrete cover shall apply as per EOTA TR 069 and EN 1992-1-1
- Working life of 50 years

For specific design cases refer to [PROFIS Engineering](#)

Rebar-size mm	Concrete class	Design Resistance (Yielding) [kN]	Cracked concrete bond resistance as per ETA			Uncracked concrete bond resistance as per ETA		
			$l_{bd,y}$ ( $C_d=3\phi$ ) [mm]	$l_{bd,y}$ ( $C_d=5\phi$ ) [mm]	$l_{bd,y}$ ( $C_d=8\phi$ ) [mm]	$l_{bd,y}$ ( $C_d=3\phi$ ) [mm]	$l_{bd,y}$ ( $C_d=5\phi$ ) [mm]	$l_{bd,y}$ ( $C_d=8\phi$ ) [mm]
$\phi 8$	C20/25	21,9	-	149	131	-	149	131
	C50/60		-	119	119	-	119	119
$\phi 10$	C20/25	34,1	-	209	113	-	209	109
	C50/60		-	108	103	-	108	100
$\phi 12$	C20/25	49,2	-	252	145	-	252	131
	C50/60		-	132	132	-	132	119
$\phi 13$	C20/25	57,7	-	288	146	-	288	130
	C50/60		-	148	146	-	148	129
$\phi 14$	C20/25	66,9	759	325	179	759	325	152
	C50/60		390	168	163	390	168	139
$\phi 16$	C20/25	87,4	970	407	212	970	407	183
	C50/60		500	210	193	500	210	158
$\phi 18$	C20/25	110,6	1180	495	244	1180	495	223
	C50/60		608	255	244	608	255	191





Rebar-size mm	Concrete class	Design Resistance (Yielding) [kN]	Cracked concrete bond resistance as per ETA			Uncracked concrete bond resistance as per ETA		
			$l_{bd,y}$ ( $c_d=3\phi$ ) [mm]	$l_{bd,y}$ ( $c_d=5\phi$ ) [mm]	$l_{bd,y}$ ( $c_d=8\phi$ ) [mm]	$l_{bd,y}$ ( $c_d=3\phi$ ) [mm]	$l_{bd,y}$ ( $c_d=5\phi$ ) [mm]	$l_{bd,y}$ ( $c_d=8\phi$ ) [mm]
φ20	C20/25	136,6	1410	592	307	1410	592	266
	C50/60		726	305	279	726	305	212
φ22	C20/25	165,3	1655	695	320	1655	695	313
	C50/60		852	358	320	852	358	233
φ24	C20/25	196,7	1765	712	358	1765	712	310
	C50/60		907	367	358	907	367	255
φ25	C20/25	213,4	1940	794	416	1940	794	349
	C50/60		998	408	378	998	408	265
φ28	C20/25	267,7	2480	1040	480	2480	1040	468
	C50/60		1275	535	436	1275	535	297
φ30	C20/25	307,3	2780	1167	570	2780	1167	525
	C50/60		1432	601	519	1432	601	342
φ32	C20/25	349,7	3100	1300	618	3100	1300	585
	C50/60		1595	670	561	1595	670	365
φ36	C20/25	442,6	3780	1585	718	3780	1585	713
	C50/60		1945	816	718	1945	816	445
φ40	C20/25	546,4	4505	1890	1070	4505	1890	850
	C50/60		2320	1070	1070	2320	973	539

The highlighted values exceed the maximum length given in ETA-20/0539 and IFU.

### Seismic loading based on ETA-20/0539. Seismic design according EOTA TR 069

All data in this section applies to:

- Hammer drilling, Hammer drilling with Hilti hollow drill bit
- working life of 50 years

For specific design cases refer to [PROFIS Engineering](#)

Rebar Size	φ8	φ10	φ12	φ13	φ14	φ16	φ18	φ20	φ22	φ24	φ25	φ28	φ30	φ32	φ36	φ40	
<b>Pull-out failure</b>																	
Reduction factor for pull-out resistance under seismic action $\alpha_{eq,p}$	[-]	0,61							0,83							0,65	
Influence of cracked concrete on bond resistance $\tau_{Rd}$																	
Factor for influence of cracked concrete $\Omega_{cr,03}$	[-]	1,00	0,96	0,90	0,88	0,85	0,82	0,78	0,76	0,73	0,71	0,70	0,68	0,66	0,65	0,62	0,60
Factor for influence of cracked concrete $\Omega_{cr,05}$	[-]	0,79	0,81	0,82	0,83	0,84	0,82	0,78	0,76	0,73	0,71	0,70	0,68	0,66	0,65	0,62	0,60
Factor for influence of cracked concrete $\Omega_{cr,08}$	[-]	0,59	0,61	0,63	0,64	0,65	0,67	0,69	0,71	0,72	0,71	0,70	0,68	0,66	0,65	0,62	0,60
<b>Bond-splitting failure</b>																	
Reduction factor for bond-splitting resistance under seismic action $\alpha_{eq,sp}$	[-]								0,95								

### Resistance to chemical substances

Chemicals tested	Content (%)	Resistance	Chemical tested	Content (%)	Resistance
Toluene	47,5	+	Sodium hydroxide 20%	100	-
Iso-octane	30,4	+	Triethanolamine	50	-
Heptane	17,1	+	Butylamine	50	-
Methanol	3	+	Benzyl alcohol	100	-
Butanol	2	+	Ethanol	100	-
Toluene	60	+	Ethyl acetate	100	-
Xylene	30	+	Methyl ethyl ketone (MEK)	100	-
Methylnaphthalene	10	+	Trichlorethylene	100	-
Diesel	100	+	Lutensit TC KLC 50	3	+
Petrol	100	+	Marlophen NP 9,5	2	+
Methanol	100	-	Water	95	+
Dichloromethane	100	-	Tetrahydrofurane	100	-
Mono-chlorobenzene	100	o	Demineralized water	100	+
Ethylacetat	50	+	Salt water	saturated	+
Methylisobutylketone	50	+	Salt spray testing	-	+
Salicylic acid-	50	+	SO <sub>2</sub>	-	+
Acetophenon	50	+	Enviroment/wheather	-	+
Acetic acid	50	-	Oil for formwork (forming oil)	100	+
Propionic acid	50	-	Concentrate plasticizer	-	+
Sulfuric acid	100	-	Concrete potash solution	-	+
Nitric acid	100	-	Concrete potash solution	-	+
Hydrochloric acid	36	-	Saturated suspension of borehole cuttings	-	+
Potassium hydroxide	100	-			

- +** Resistant
- Not resistant
- o** Partially Resistant



## Setting information

### Installation temperature range

-5 °C to +40 °C

### Service temperature range

Hilti HIT-RE 500 V4 injection mortar may be applied in the temperature ranges given below. An elevated base material temperature may lead to a reduction of the design bond resistance.

#### ETA-20/0540

Temperature range	Base material temperature	Maximum long term base material temperature	Maximum short term base material temperature
Temperature range I	-40 °C to +80 °C	+50 °C	+80 °C

#### ETA-20/0539

Temperature range	Base material temperature	Maximum long term base material temperature	Maximum short term base material temperature
Temperature range I	-40 °C to +40 °C	+24 °C	+40 °C
Temperature range II	-40 °C to +55 °C	+43 °C	+55 °C
Temperature range III	-40 °C to +75 °C	+55 °C	+75 °C

### Maximum short term base material temperature

Short-term elevated base material temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling.

### Maximum long term base material temperature

Long-term elevated base material temperatures are roughly constant over significant periods of time.

### Working time and curing time<sup>1) 2)</sup>

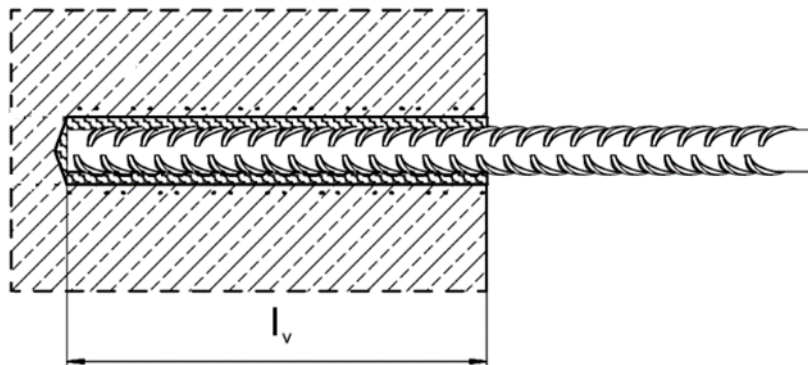
Temperature of the base material	Maximum working time	Initial curing time	Minimum curing time
T <sup>2)</sup>	t <sub>work</sub>	t <sub>cure,ini</sub>	t <sub>cure</sub>
-5 °C to -1 °C	2 h	48 h	168 h
> -1 °C to 4 °C	2 h	24 h	48 h
> 5 °C to 9 °C	2 h	16 h	24 h
> 9 °C to 14 °C	1,5 h	12 h	16 h
> 14 °C to 19 °C	1 h	8 h	16 h
> 19 °C to 24 °C	30 min	4 h	7 h
> 24 °C to 29 °C	20 min	3,5 h	6 h
> 29 °C to 34 °C	15 min	3 h	5 h
> 34 °C to 39 °C	12 min	2 h	4,5 h
> 39 °C to 40 °C	10 min	2 h	4 h

<sup>1)</sup> The curing time data are valid for dry base material only. In wet base material, the curing times must be doubled.

<sup>2)</sup> The minimum temperature of the foil pack is +5° C.

Dispenser and corresponding maximum embedment depth  $l_{v,max}$

Rebar size	HDM 330, HDM 500	HDE 500	HIT-P8000D
	$l_{v,max}$ [mm]		
φ8	1000	1000	-
φ10		1000	-
φ12		1200	1200
φ13		1300	1300
φ14		1400	1400
φ16		1600	1600
φ18	700	1800	1800
φ20	600	2000	2000
φ22	500	1800	2200
φ24	300	1300	2400
φ25	300	1500	2500
φ26	300	1000	2600
φ28	300	1000	2800
φ30	-	1000	3000
φ32		700	3200
φ34		600	
φ36		600	
φ40		400	














For detailed setting information on installation see instructions for use given with the product.

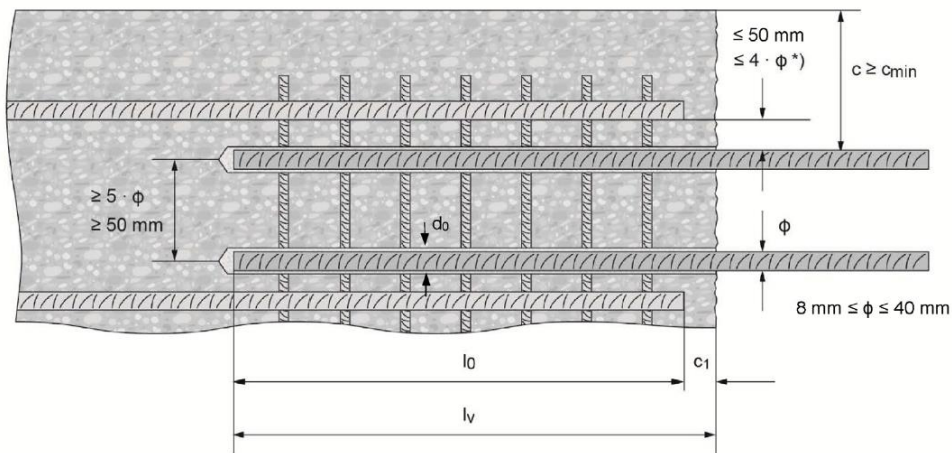
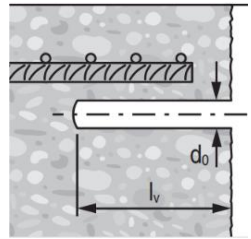
Approved installation methods can be found in the specific ETA/Certificate definitions.

**Drilling and Installation equipment**

Rotary Hammers (Corded and Cordless)		TE 2 - TE 70
Diamond Coring Machines		DD EC-1, DD 100 ... DD 160
Dispenser		HDE HDM PE-8000D
Other tools		Blow out pump, Compressed air gun Set of cleaning brushes
		Hammer drill bit TE-CX, TE-YX, TE-C, TE-Y
		Hollow drill bit TE-CD, TE-YD
		Diamond core bit SP-L, SP-HX, SP-H, P-U
		Roughening tools TE-YRT
		Piston plug

**Minimum concrete cover  $c_{min}$  of the post-installed rebar**

Drilling method	Bar diameter [mm]	Minimum concrete cover $c_{min}$ [mm]	
		Without drilling aid	With drilling aid
Hammer drilling (HD) and (HDB)	$\phi < 25$	$30 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$30 + 0,02 \cdot l_v \geq 2 \cdot \phi$
	$\phi \geq 25$	$40 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$40 + 0,02 \cdot l_v \geq 2 \cdot \phi$
Compressed air drilling (CA)	$\phi < 25$	$50 + 0,08 \cdot l_v$	$50 + 0,02 \cdot l_v$
	$\phi \geq 25$	$60 + 0,08 \cdot l_v \geq 2 \cdot \phi$	$60 + 0,02 \cdot l_v \geq 2 \cdot \phi$
Diamond coring with roughening with Hilti Roughening tool TE-YRT (RT)	$\phi < 25$	$30 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$30 + 0,02 \cdot l_v \geq 2 \cdot \phi$
	$\phi \geq 25$	$40 + 0,06 \cdot l_v \geq 2 \cdot \phi$	$40 + 0,02 \cdot l_v \geq 2 \cdot \phi$



<sup>\*)</sup> If the clear distance between lapped bars exceeds  $4 \cdot \phi$  or 50 mm, then the lap length shall be increased by the difference between the clear bar distance and the smaller of  $4 \cdot \phi$  or 50 mm.

Where,  $c$  is concrete cover of post-installed rebar

$c_1 = c_r$  is the end-cover of existing rebar

$d_0$  is the nominal drill bit diameter

$\phi$  diameter of reinforcement bar

$l_0$  is the lap length

$l_v$  is the installation length